

## Utilizing Unified Power Flow Controller for Voltage Stability Improvement of the Electric Power Transmission System of Ghana

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**Abstract**— Interconnecting power transmission systems provide reliability of electric power supply. The security of the system is however questioned when a disturbance in any part of the interconnected system causes instability in the entire network. Unified Power Flow Controller (UPFC), which is a member of the flexible alternating current transmission system (FACTS) family, has the capability of controlling active and reactive power flow in a transmission line thereby improving the voltage stability of the system especially at the 500 kV configuration level. The performance of a 161-kV UPFC modelled in SimPowerSystems is tested on Ghana's power transmission network. The optimal placement of the UPFC is done using fast voltage stability index (FVSI) and maximum loadability assessment (MLA). The results show that the device improved the connecting bus voltage from 0.88 p.u. to 0.98 p.u. Active power loss in the network was also reduced from 13.40 MW to 10.39 MW when the UPFC was in circuit.

*Keywords: Ghana, Stability, Transmission system and Unified Power Flow Controller (UPFC)*

### 1. Introduction

As demand in electricity grows, there is the need for more interconnections of power transmission systems. These complex interconnections provide low cost on power transmission and reliability [1]. Along with the positive impacts are the negative effects which threaten the reliability and security of these interconnected systems [2]. The authors in [3] identified the major problem associated with a power transmission system to be instability, where, a disturbance in any part of the power system may lead to either partial or total system collapse. The instability is determined based on the parameters affecting the power system. These can be categorised under rotor angle, frequency and voltage stability [4]. Even as frequency and rotor angle can be controlled locally from the generating stations, the action of over exciter limiters (OEL) prevents a complete control of voltage stability [5]. Voltage instability has caused a number of outages in power systems world-wide, and has been documented by [6].

A number of methods used to solve voltage stability problems have been discussed by [7], [8]. Among these methods are: coordination of

protection and control systems, reactive power compensating devices, tap changing transformers, and operating an adequate reserve margin. Reactive power compensation through the use of flexible alternating current transmission system (FACTS) devices has become the most effective means of improving voltage stability of an interconnected power system [9]. FACTS devices have recently been used widely in weak power systems. They can control power flow during normal and abnormal operating conditions with the capability of improving system voltages by reducing power losses. The effect of these devices should however be assessed prior to their use to help achieve the optimum operating results [10].

A series of FACTS devices (SSSC and TCSC) to improve power system stability on a 500-kV transmission line were implemented in [11]. The performance results of the implemented devices however demonstrated an unstable steady state condition without a power system stabilizer. The authors in [12] demonstrated the performance of different FACTS devices on an IEEE 9-bus system. The modelled network was subjected to a 3-phase symmetrical fault. The results indicated that the shunt connected devices increased the

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are both coupled to a common DC link capacitor. A switch is connected between both sets of capacitors to enable the UPFC to operate in several modes. The opening and closing of the switch cause the device to either assume operation in the STATCOM, SSSC or UPFC mode. With both converters able to transfer active and reactive power through the common DC link capacitor, the injected voltage generated by the SSSC is not limited to stay in quadrature with the line current but can rather assume any angle with respect to the current, making it possible to transfer or absorb active and reactive power as well as to improve system voltages.

### 3. Description of Test System

The test system is modelled as the power system present at the northern section of Ghana's transmission network. The system consists of two generating sources and also contains 1090.4 circuit kilometers of 161 kV transmission lines interconnecting eleven bulk supply points (BSPs) with 17 MVar static capacitor banks at four different BSPs. This helps to verify the effectiveness of these devices on the improvement of voltage on the actual system.

### 4. Methodology

System data taken from Ghana's grid was used to model the power system in MATLAB Simscape

Power Systems software (SimPowerSystems).

An overview of the software is presented by [24]. The system data is entered into the pre-modelled blocks of the software to depict the actual system. After the power system has been modelled, load flow analysis is performed to determine the state of the network before compensation. The power and control circuits of the UPFC are also modelled using the same software.

The high-power control of the 161-kV network is achieved by using four GTO based square wave inverters of 100 MVA at each side of a common DC link capacitor. The voltage produced by each inverter is applied to four phase-shifting transformers (each connected to one inverter) to eliminate harmonics to the 45<sup>th</sup> level. The nominal power on each transformer is selected at 25 MVA at a frequency of 50 Hz and a turns ratio of 9.5. With a surge impedance loading of 100 MVA and a voltage of 161 kV, the phase current derived is 358.6 A, which helps to determine the DC link capacitor rating as 4000  $\mu$ F. The UPFC controller is designed in accordance with the description provided by [25]. The complete system model with UPFC optimally located is found in Fig 2.

To verify the results obtained from placing the UPFC at the optimal location, a modelled STATCOM is placed at the same location where the UPFC is placed and a comparison is made on their results.

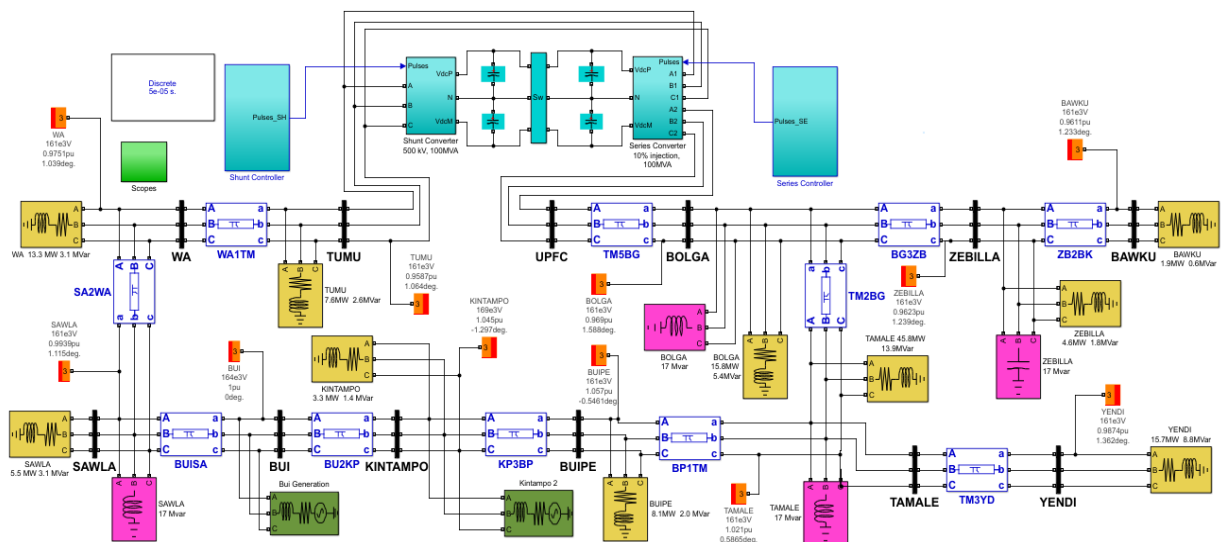


Fig. 2 The complete power transmission system model of the UPFC optimally located

The optimal location of the UPFC is done by finding the weakest bus and the critical lines in the network. The weakest bus is identified using MLA by determination of maximum reactive power that each load bus in the network can tolerate without network collapse. In this regard, the bus with the least value of maximum reactive power is considered as the weakest bus. The adjoining critical line is determined using the FVSI. This index is determined using equation (1) as proposed by [26].

$$\frac{4Q_r Z^2}{V_s^2 X} \leq 1 \quad (1)$$

where,  $Q_r$  is receiving end reactive power in MVAR,  $Z$  is line impedance in ohms,  $V_s$  is sending end voltage in volts,  $X$  is line reactance in ohms.

The UPFC is then placed at the point where the critical line meets the weakest bus. The flowchart of Fig. 3 describes the procedure in determining the optimal location of the UPFC.

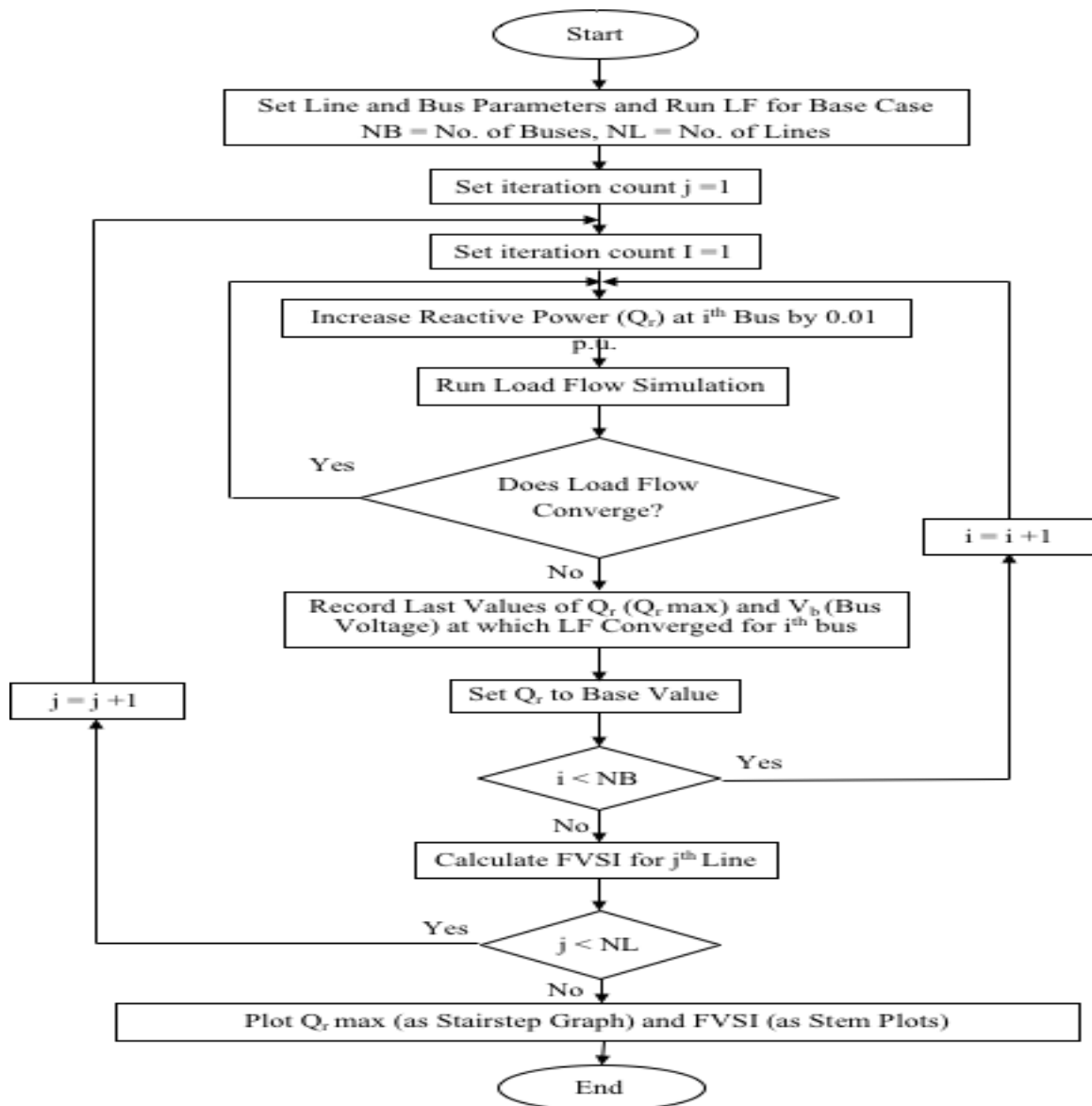


Fig. 3 Flowchart used to determine optimal location of UPFC

A write-up of the flowchart is as follows:

*Step 1:* Load system data and perform initial load flow studies for base case.

*Step 2:* Select one bus and progressively increase its reactive power by 0.01 MVAR.

*Step 3:* Perform load flow studies for each increment until load flow solution fails to converge

*Step 4:* Record the last value of reactive power increment ( $Q_r$ ) and its corresponding adjoining bus voltage, ( $V_s$ ) at which load flow converges.

This indicates the maximum reactive power (maximum loadability), above which voltage collapse may occur on the said bus.

*Step 5:* Repeat steps (ii) to (iv) until all buses have been selected.

*Step 6:* Insert  $Q_r$  and  $V_s$  into (1) and determine the FVSI for each line

*Step 7:* Sort the maximum loadability,  $Q_r$  in ascending order. The bus with the least value is ranked the weakest bus.

*Step 8:* The line with the highest value of FVSI is the most critical line, which is capable of causing voltage collapse.

### 5. Results and Discussions

The results obtained from simulating the modelled system are presented in this section. The FVSI and MLA results are presented in Table 1 and Fig. 4 shows the outcome of load flow voltages with UPFC, STATCOM and with no device in circuit.

Table 1. Results of FVSI and MLA

Line	Line ID	FVSI	Bus	MLA(Mvar)
Kintampo - Buipe	KP3BP	0.0934	BUIPE	2452
Buipe - Tamale	BP1TM	0.1548	TAMALE	546
Tamale - Bolga	TM2BG	0.0846	BOLGA	14.4
Bui - Sawla	BU1SA	0.0357	SAWLA	54.1
Tamale - Yendi	TM3YD	0.0298	YENDI	24.9
Bolga - Zebilla	BG3ZB	0.0074	ZEBILLA	10.9
Zebilla - Bawku	ZB2BK	0.0050	BAWKU	9.1
Sawla - Wa	SA2WA	0.2550	WA	2211
Wa - Tumu	WA1TM	0.5800	TUMU	8.6
Tumu - Bolga	TM5BG	0.0178		

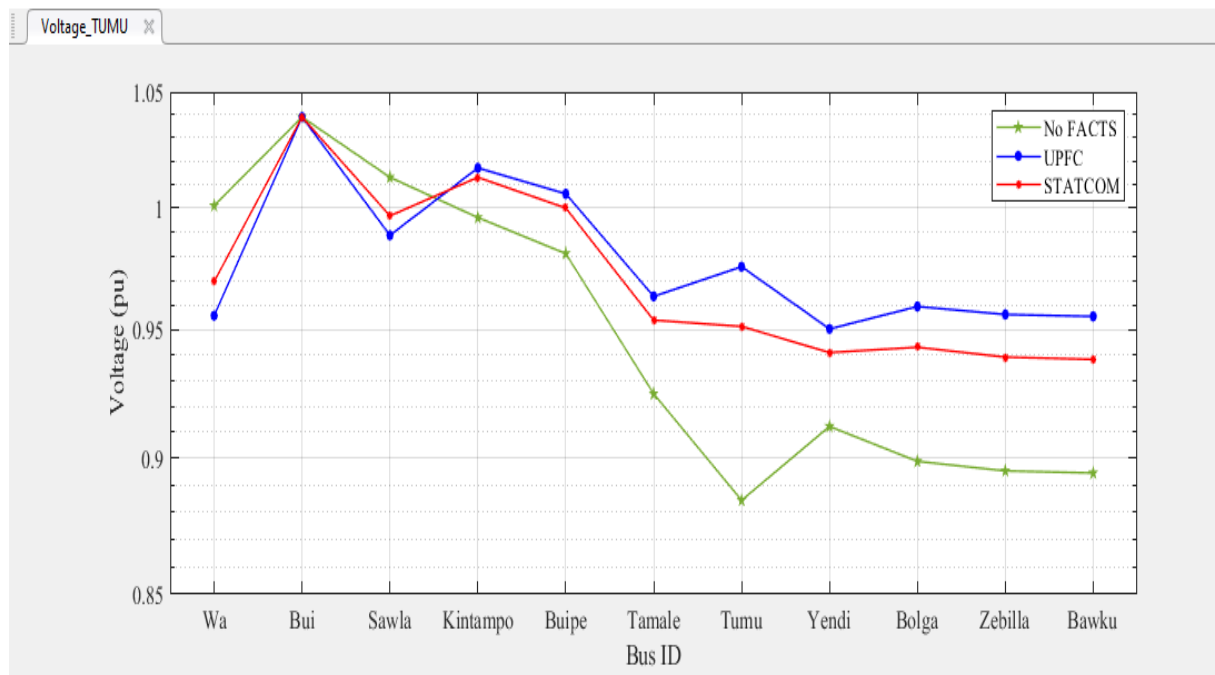


Fig. 4 Results of voltage profile with UPFC, STATCOM and with no device in circuit

From Table 1, a conclusion can be drawn that the TUMU bus, which is the weakest and also linking the critical line is suitable for the placement of the UPFC. The UPFC is placed at the optimal location and series of simulations are performed to determine its performance.

As evident from Fig. 4, the UPFC produced voltage levels within a stability limit of 5% p.u. for all buses in the network. The bus voltage at Tumu improved significantly from 0.8843 p.u. to 0.9756 p.u. The lowest bus p.u. voltage of 0.9504 recorded in the network for the UPFC is found at Yendi. This lowest value at Yendi was as a result of the radial line connecting

the Yendi bus, and more importantly, this bus is most distant from the Tumu BSP. When the STATCOM was connected to the same bus, four of its buses (Yendi, Bolga, Zebilla and Bawku) had voltages below the stability limit of 5% p.u.

Fig 5 presents the results on active power loss for all three scenarios. With no FACTS device connected, the active power loss in the system was 13.40 MW. Connecting the STATCOM to the system reduced the power loss to 12.16 MW, whilst the UPFC gave a better improvement by further reducing the active power loss to 10.39 MW

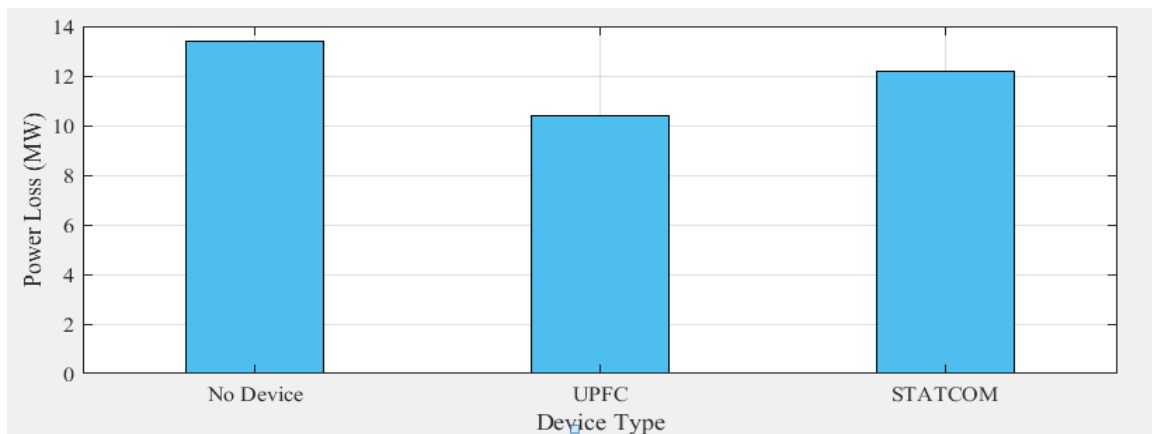


Fig. 5 Active power loss of the system with and without FACTS devices

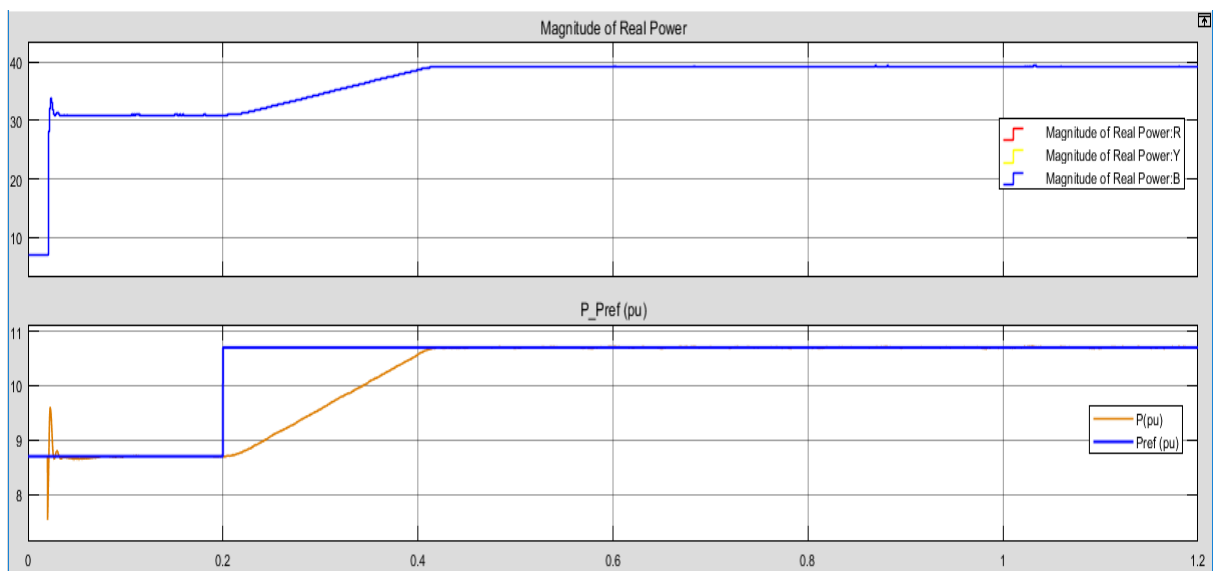


Fig. 6 Simulation results on active power flow control of the UPFC

The performance of the UPFC controllers are also verified using simulations. Scopes were connected at various outputs to interpret the results on each controller. In the power flow control mode, the active power flow on the network bus linking the UPFC bus was realised to be 5.4 MW. At time 0.025s, when the UPFC was brought into circuit, the power capability of the connecting line increased to 32.50 MW as can be seen in the first trace of Fig. 6.

A step change introduced into the reference

power from 8.7 p.u. to 10.7 p.u. at 0.2s causes the UPFC to respond by increasing the active power transfer from 32.50 MW to 40 MW.

The action of the reactive power controller is similar to the active power controller. From Fig 7, the UPFC initially produced a reactive power control of 3.4 MVar. A step change introduced to the reactive power controller caused the UPFC to increase its reactive power transfer to 7.8 MVar on the connecting bus.

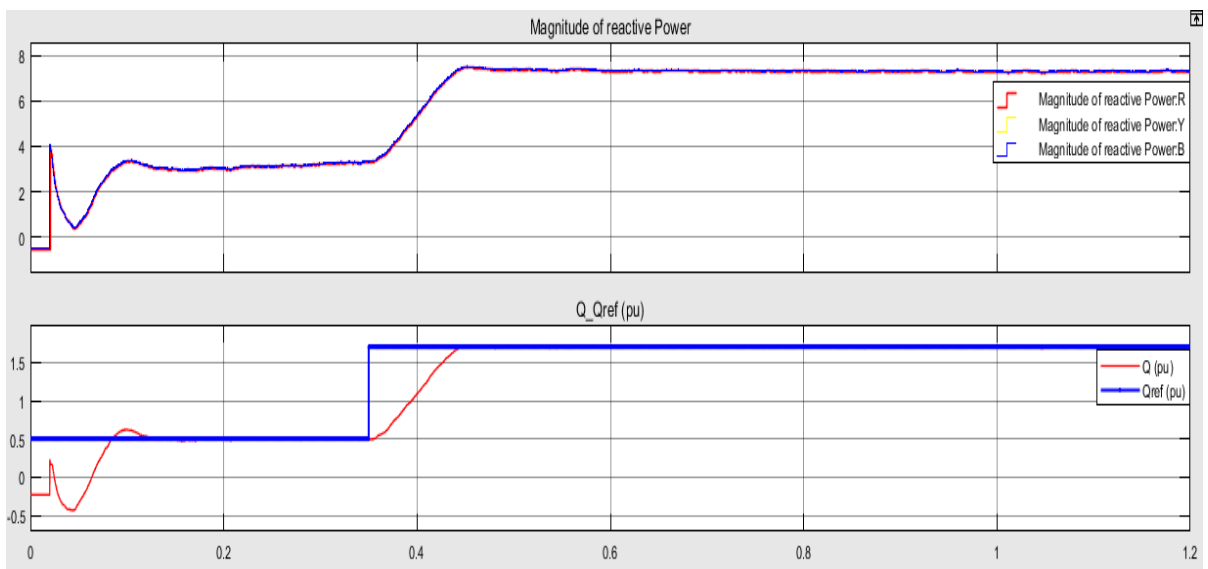


Fig. 7 Simulation results on reactive power flow control of the UPFC

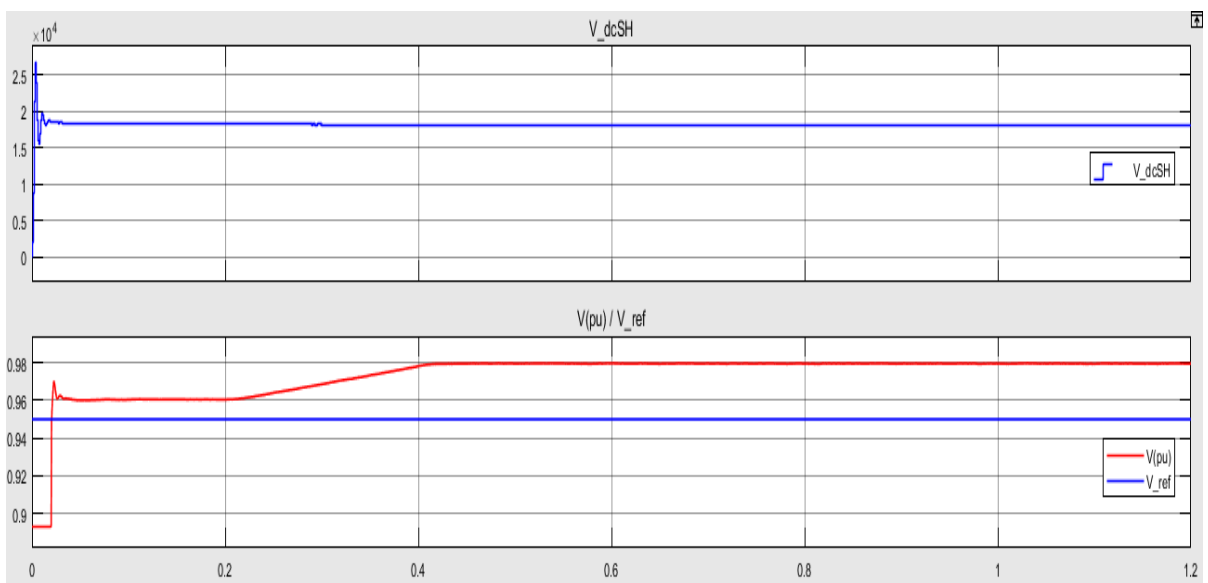


Fig. 8 Simulation results on bus voltage and shunt side DC voltage

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The voltage improvement of the network is achieved by the STATCOM and UPFC controllers. At the start of the simulations, the voltage realised on the connecting bus was 0.89 p.u. and the initial action of the UPFC increased the bus voltage to 0.96 p.u. When the active power flow on the line was increased, the voltage level on the connecting bus also increased to a new value of 0.98 p.u. as found in Fig. 8.

It is evident from the results that an increase in active power transfer on a transmission line has a positive effect on bus voltage. The DC capacitor voltage on the shunt side remained constant throughout the entire simulations.

## 6. Conclusion

A 161-kV configuration of an UPFC was successfully modelled using SimPowerSystems. The device was optimally placed using FVSI and MLA. Connecting the UPFC in circuit produced voltage levels within a stability limit of 5% p.u. for all buses in the network. The active power loss in the system was significantly reduced from 13.40 MW to 10.39 MW when the UPFC was placed in circuit.

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